

一类随机系统基于自适应非线性 干扰观测器的抗干扰控制

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摘要: 本文针对一类带有多源异质干扰的随机系统研究了抗干扰控制问题. 多源异质干扰包括与系统状态和控制输入耦合的未知非谐波扰动和白噪声. 设计了自适应非线性干扰观测器用来估计非谐波扰动. 在此基础上, 提出了一种基于自适应非线性干扰观测器的抗干扰控制方法. 最后通过仿真算例验证了所提策略的有效性.

关键词: 随机系统; 多源异质干扰; 抗干扰控制; 自适应非线性干扰观测器

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不同来源、不同渠道的干扰广泛存在, 影响系统的性能. 因此需要有效的控制方法来抑制和抵消干扰. 作为一种重要的控制方法, 基于干扰观测器的控制方法(DOBC)于20世纪80年代末被提出, 其基本思想是通过构造干扰观测器在线估计干扰, 以干扰观测器的输出为基础, 将传统的反馈控制器和前馈补偿器进行结合以实现干扰补偿的目标. 近年来, DOBC在随机系统的研究也受到了广泛的关注. Wei等^[1]首次将DOBC方法推广到一类多扰动随机系统, 提出了一种基于干扰观测器的干扰衰减控制方法, 以保证复合系统渐近均方有界. Sun等^[2]研究了带有部分信息已知的干扰和白噪声的随机马尔可夫跳变系统的干扰衰减和抑制问题, 提出了一种基于扰动观测器的衰减抑制控制器, 使闭环系统在不同条件下均方有界或渐近稳定. Wei等^[3]针对带有多扰动和非线性的离散时间随机系统, 提出了复合分层抗干扰控制策略, 保证了闭环系统依均方渐近稳定.

另一方面, 最近研究的干扰通常是由线性外生系统描述, 表示一类谐波或中立稳定的干扰^[4-5], 然而在实际应用中非谐波干扰也是广泛存在的^[6-8]. 一些研究假设非谐波干扰是非线性函数或是范数有界的^[9-11]. Wang等^[12]针对一类由外生系统产生扰动的非线性系统, 提出了基于非线性扰动观测器的控制方法. Dong等^[13]针对一类具有非谐波扰动的随机系统, 提出了基于非线性干扰观测器的扰动衰减控制方案. 以上文献研究的非谐波干扰是已知的并且与干扰状态有关. Li等^[14]考虑部分未知马尔可夫跳变参数的非线性奇异随机混合系统的复合抗扰动弹性控制, 其中所研究的非线性扰动是未知的, 用系统状态表示. 然而, 与系统状态和控制输入耦合的未知非谐波干扰在工程应用中是普遍存在的^[8, 15-16], 现有的抗干扰控制方案难以达到预期的控制性能.

本文为解决一类带有多源异质干扰的随机系统的抗干扰控制问题, 提出一种基于自适应非线性干扰观测器的抗干扰控制策略. 若考虑具有复杂非线性特征的未知非谐波干扰和白噪声, 现有的DOBC策略很难有效处理未知的非谐波干扰, 因此将DOBC方法和自适应技术结合, 设计自适应非线性干扰观测器来估计非谐波干扰, 进而提出基于自适应非线性干扰观测器的控制方案, 使得复合系统达到想要的控制性能.

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1 问题描述

一类带有多源异质干扰的随机系统描述如下:

$$\dot{x}(t) = A_0 x(t) + B_0 [u(t) + D(t)] + B_1 x(t) \xi(t), \quad (1)$$

式中: $x(t) \in \mathbf{R}^n$, $\mu \in \mathbf{R}^m$ ($m < n$) 分别是系统状态和控制输入; $\xi(t)$ 是白噪声; $A_0 \in \mathbf{R}^{n \times n}$, $B_0 \in \mathbf{R}^{n \times m}$, $B_1 \in \mathbf{R}^n$ 是常数矩阵. $D(t) \in \mathbf{R}^m$ 为非谐波干扰, 干扰系统描述如下:

$$\begin{cases} D(t) = V\omega(t), \\ \dot{\omega}(t) = G\omega(t) + f(\omega(t), x(t), \mu(t)) + H_1 \delta_1(t), \end{cases} \quad (2)$$

式中: $\omega(t) \in \mathbf{R}^m$ 是干扰系统的状态; G, V 是已知的常数矩阵; $f(\omega(t), x(t), \mu(t))$ 是未知的非线性函数; $\delta_1(t)$ 是由不确定性造成的附加扰动. $D(t)$ 代表着更广泛的干扰模型, 是与系统状态、控制输入、附加扰动有关的非谐波干扰.

根据文献 [17], 由 $\frac{dW(t)}{dt}$ 代替 $\xi(t)$, 系统 (1) 和 (2) 等价于以下系统:

$$dx(t) = A_0 x(t) dt + B_0 [u(t) + D(t)] dt + B_1 x(t) dW(t), \quad (3)$$

$$\begin{cases} D(t) = V\omega(t), \\ d\omega(t) = G\omega(t) dt + f(\omega(t), x(t), \mu(t)) dt + H_1 \delta_1(t) dt, \end{cases} \quad (4)$$

其中, $W(t)$ 是定义在完备概率空间 $(\Omega, \mathcal{F}, \mathcal{F}_t, P)$ 上的独立标准维纳过程(布朗运动).

假设 1 存在未知的常数 c_i ($i = 1, 2, 3, 4$), 使得非线性函数 $f(\omega(t), x(t), \mu(t))$ 满足

$$\|f(\omega(t), x(t), \mu(t))\| \leq c_1 + c_2 \|\omega(t)\| + c_3 g_1(x(t), \mu(t)) + c_4 \|g_2(x(t), \mu(t))\|, \quad (5)$$

式中: $g_1(x(t), \mu(t))$ 和 $g_2(x(t), \mu(t))$ 是已知的非负函数, $\|\cdot\|$ 表示向量的欧几里德范数.

根据参考文献 [15] 和 [16] 可知, 假设 1 是未知非线性函数满足的一般条件. 对于非谐波干扰的研究往往是包含满足 Lipschitz 条件的非线性函数^[9, 13], 这是作为假设 1 的一种特殊情况.

假设 2 (A_0, B_0) 为能控的.

考虑以下随机微分方程:

$$dx(t) = f(x(t), t) dt + g(x(t), t) dB(t), \quad t \geq t_0, \quad (6)$$

式中: $f: \mathbf{R}^n \times \mathbf{R}_+ \rightarrow \mathbf{R}^n$, $g: \mathbf{R}^n \times \mathbf{R}_+ \rightarrow \mathbf{R}^{n \times m}$ 满足局部 Lipschitz 条件, 且 $f(0, t) = 0$, $g(0, t) = 0$, $B(t)$, $t \geq 0$ 是一个 m 维独立维纳过程.

定义 1^[18] 设 $p > 0$, 系统 (6) 是依 p 阶概率有界, 若存在正常数 H , 对所有的 $(t_0, x_0) \in \mathbf{R}_+ \times \mathbf{R}^n$, 满足

$$\limsup_{t \rightarrow \infty} E \|x(t; t_0, x_0)\|^p \leq H. \quad (7)$$

当 $p = 2$ 时, 系统 (6) 满足依均方渐近有界.

引理 1^[18] 假设存在函数 $V(x, t)$ 满足 $k_1(\|x\|) \leq V(x, t) \leq k_2(\|x\|)$, $k_1(\cdot), k_2(\cdot)$ 是 k_∞ 类函数, 存在正常数 p, ρ, λ , 使得对所有的 $(t_0, x_0) \in \mathbf{R}_+ \times \mathbf{R}^n$, 满足

$$k(\|x\|^p) \leq V(x, t), \quad LV(x, t) \leq -\lambda V(x, t) + \beta, \quad (8)$$

其中: $LV(x, t)$ 是一个微分算子, 定义为

$$LV(x, t) = \frac{\partial V}{\partial t} + \frac{\partial V}{\partial x} f(x, t) + \frac{1}{2} \text{Tr} \{ g(x, t)^T \frac{\partial^2 V}{\partial x^2} g(x, t) \}, \quad (9)$$

即对所有的 $(x, t) \in \mathbf{R}^n \times \mathbf{R}_+$ 有

$$\limsup_{t \rightarrow \infty} E \|x(t; t_0, x_0)\|^p \leq k^{-1} \left(\frac{\beta}{\lambda} \right), \quad (10)$$

那么, 系统 (6) 是依 p 阶渐近有界的.

2 自适应非线性干扰观测器

假设系统状态 $x(t)$ 是可以通过测量获得, 干扰观测器构造如下:

$$\begin{cases} \hat{D}(t) = V\hat{\omega}(t), \\ dz(t) = A_0 z(t) dt + B_0 [u(t) + D(t)] dt + L_0 [x(t) - z(t)] dt, \\ d\hat{\omega}(t) = G\hat{\omega}(t) dt + L_1 [x(t) - z(t)] dt + \beta(t) [x(t) - z(t)] \varphi(\hat{\omega}(t), x(t), \mu(t)) dt, \end{cases} \quad (11)$$

$\beta(t)$ 是自适应律, 由下列的更新律更新

$$\dot{\beta}(t) = \eta (\|x(t) - z(t)\|^2 \varphi(\hat{\omega}(t), x(t), \mu(t)) - \alpha \beta(t)), \quad (12)$$

式中: $D(t)$ 和 $\omega(t)$ 的估计值分别为 $\hat{D}(t)$ 和 $\hat{\omega}(t)$; L_0 和 L_1 是观测器增益; $z(t)$ 是辅助变量作为观测器的状态; $\eta, \alpha > 0$ 是设计参数; $\varphi(\hat{\omega}(t), x(t), \mu(t))$ 是非线性函数, 定义如下

$$\begin{aligned} \varphi(\hat{\omega}(t), x(t), \mu(t)) = \\ 2 + \|\hat{\omega}(t)\|^2 + g_1^2(x(t), \mu(t)) + g_2^2(x(t), \mu(t)) + \|\hat{\omega}(t)\|^2 g_2^2(x(t), \mu(t)). \end{aligned} \quad (13)$$

干扰误差 $e_s(t) = x(t) - z(t)$, $e_\omega(t) = \omega(t) - \hat{\omega}(t)$, 根据式 (3)、(4) 和 (11) 得到以下误差系统:

$$de_s(t) = (A_0 - L_0) e_s(t) dt + B_0 V e_\omega(t) dt + B_1 x(t) dW(t), \quad (14)$$

$$\begin{aligned} de_\omega(t) = G e_\omega(t) dt - L_1 e_s(t) dt - \beta(t) e_s(t) \varphi(\hat{\omega}(t), x(t), \mu(t)) dt + \\ f(\omega(t), x(t), \mu(t)) dt + H_1 \delta_1(t) dt. \end{aligned} \quad (15)$$

通过设计观测器增益和自适应律使得式 (14) 和 (15) 达到理想的控制性能.

控制器设计如下:

$$u(t) = Kx(t) - \hat{D}(t). \quad (16)$$

将 (16) 式代入 (3) 式中得到闭环系统:

$$dx(t) = (A_0 + B_0 K) x(t) dt + B_0 V e_\omega(t) dt + B_1 x(t) dW(t). \quad (17)$$

将式 (14)、(15) 和 (17) 式结合在一起, 令 $\bar{x}(t) = [x(t) \quad e_s(t) \quad e_\omega(t)]^T$, $\delta(t) = [0 \quad 0 \quad \delta_1(t)]^T$, 得到复合系统:

$$\begin{cases} d\bar{x}(t) = A\bar{x}(t) dt + H\delta(t) dt + B\bar{x}(t) dW(t) - \beta(t) E e_s(t) \varphi(\hat{\omega}(t), x(t), \mu(t)) dt + \\ \quad E f(\omega(t), x(t), \mu(t)) dt, \\ y(t) = C\bar{x}(t), \end{cases} \quad (18)$$

其中 $y(t)$ 是参考输出, $C = [C_1 \quad C_2 \quad C_3]$ 是加权矩阵且

$$A = \begin{bmatrix} A_0 + B_0 K & 0 & 0 \\ 0 & A_0 - L_0 & B_0 V \\ 0 & -L_1 & G \end{bmatrix}, H = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & H_1 \end{bmatrix}, B = \begin{bmatrix} B_1 & 0 & 0 \\ B_1 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}, E = \begin{bmatrix} 0 \\ I \\ 0 \end{bmatrix}.$$

3 基于自适应非线性干扰观测器的抗干扰控制

本节目的是设计自适应非线性干扰观测器的抗干扰控制策略, 使复合系统达到期望的动态性能.

定理 1 基于假设 1~2, 对带有干扰 $D(t)$ 的随机系统 (1), 若存在矩阵 $X > 0$, $Q_2 > 0$, $Q_3 > 0$, 且有常数 $\tau > 0$, 矩阵 R_1, R_2, R_3 满足

$$\Omega = \begin{bmatrix} \Lambda_1 & 0 & 0 & XB_1^T & XB_1^T & XC_1^T & 0 & 0 & 0 \\ * & \Lambda_2 & Q_2 B_0 V - R_3 & 0 & 0 & C_2^T & 0 & 0 & 0 \\ * & * & \Lambda_3 & 0 & 0 & C_3^T & 0 & 0 & Q_3 H_1 \\ * & * & * & -X & 0 & 0 & 0 & 0 & 0 \\ * & * & * & * & -Q_2 & 0 & 0 & 0 & 0 \\ * & * & * & * & * & -I & 0 & 0 & 0 \\ * & * & * & * & * & * & -\tau^2 I & 0 & 0 \\ * & * & * & * & * & * & * & -\tau^2 I & 0 \\ * & * & * & * & * & * & * & * & -\tau^2 I \end{bmatrix} < 0, \quad (19)$$

其中

$$\Lambda_1 = A_0 X + X A_0^T + B_0 R_1 + R_1^T B_0^T,$$

$$\Lambda_2 = A_0^T Q_2 + Q_2 A_0 - R_2^T - R_2,$$

$$\Lambda_3 = G^T Q_3 + Q_3 G.$$

设计自适应非线性干扰观测器(11)中的 $L_0 = Q_2^{-1} R_2$, $L_1 = (R_3 Q_3^{-1})^T$, 得到控制器(16)中的 $K = R_1 X^{-1}$, 保证复合系统(18)是依均方渐近有界.

证明 考虑如下 Lyapunov 函数:

$$V(\bar{x}(t), t) = \frac{1}{2} \bar{x}^T(t) P \bar{x}(t) + \frac{1}{2} \eta^{-1} (\beta(t) - \beta^*)^2, \quad (20)$$

其中 β^* 是一个常数, 满足 $\beta^* \geq \max\{c_2 \rho_1, c_2 \rho_4\} / 2$.

定义一个正定对角矩阵 P

$$P = \begin{bmatrix} Q_1 & 0 & 0 \\ 0 & Q_2 & 0 \\ 0 & 0 & Q_3 \end{bmatrix} = \begin{bmatrix} X^{-1} & 0 & 0 \\ 0 & Q_2 & 0 \\ 0 & 0 & Q_3 \end{bmatrix} > 0, \quad (21)$$

$$PE = N, N = [0 \quad I \quad 0], e_\varepsilon(t) = N^T \bar{x}(t).$$

复合系统在 $\delta(t) = 0$ 的情况下

$$\begin{aligned} LV(\bar{x}(t), t) &= \frac{1}{2} \bar{x}^T(t) (A^T P + PA) \bar{x}(t) - \beta(t) \bar{x}^T(t) P E e_\varepsilon(t) \varphi(\hat{\omega}(t), x(t), \mu(t)) + \\ &\bar{x}^T(t) P E f(\omega(t), x(t), \mu(t)) + \frac{1}{2} \text{Tr}(\bar{x}^T(t) B^T P B \bar{x}(t)) + \eta^{-1} (\beta(t) - \beta^*) \dot{\beta}(t) \leq \\ &\frac{1}{2} \bar{x}^T(t) [A^T P + PA + B^T P B] \bar{x}(t) - \beta(t) \|e_\varepsilon(t)\|^2 \varphi(\hat{\omega}(t), x(t), \mu(t)) + \|e_\varepsilon(t)\| [c_1 + c_2 \|\omega(t)\| + \\ &c_3 g_1(x(t), \mu(t)) + c_4 \|\omega(t)\| g_2(x(t), \mu(t))] + \eta^{-1} (\beta(t) - \beta^*) \dot{\beta}(t). \end{aligned} \quad (22)$$

由 $\|\omega(t)\| \leq \|e_\omega(t)\| + \|\hat{\omega}(t)\|$, (12) 和 (13) 得

$$\begin{aligned} LV(\bar{x}(t), t) &\leq \frac{1}{2} \bar{x}^T(t) [A^T P + PA + B^T P B] \bar{x}(t) + \|e_\varepsilon(t)\| [c_1 + c_2 \|e_\omega(t)\| + c_2 \|\hat{\omega}(t)\| + \\ &c_3 g_1(x(t), \mu(t)) + c_4 \|e_\omega(t)\| g_2(x(t), \mu(t)) + c_4 \|\hat{\omega}(t)\| g_2(x(t), \mu(t))] - \\ &\beta^* \|e_\varepsilon(t)\|^2 \varphi(\hat{\omega}(t), x(t), \mu(t)) - \alpha \beta(t) (\beta(t) - \beta^*) \leq \\ &\frac{1}{2} \bar{x}^T(t) \Omega_0 \bar{x}(t) + \|e_\varepsilon(t)\| [c_1 + c_2 \|e_\omega(t)\| + c_2 \|\hat{\omega}(t)\| + c_3 g_1(x(t), \mu(t)) + \\ &c_4 \|e_\omega(t)\| g_2(x(t), \mu(t)) + c_4 \|\hat{\omega}(t)\| g_2(x(t), \mu(t))] - \\ &\beta^* \|e_\varepsilon(t)\|^2 \varphi(\hat{\omega}(t), x(t), \mu(t)) - \alpha \beta(t) (\beta(t) - \beta^*). \end{aligned} \quad (23)$$

根据文献[19]中的 Young's 不等式, 对任意的 $\rho_1, \rho_2 > 0$ 有

$$c_2 \| e_\varepsilon(t) \| \| e_\omega(t) \| \leq \frac{1}{2} c_2 (\rho_1 \| e_\varepsilon(t) \|^2 + \frac{1}{\rho_1} \| e_\omega(t) \|^2),$$

$$c_4 \| e_\varepsilon(t) \| \| e_\omega(t) \| g_2(x(t), \mu(t)) \leq \frac{1}{2} c_4 (\rho_2 \| e_\varepsilon(t) \|^2 g_2^2(x(t), \mu(t)) + \frac{1}{\rho_2} \| e_\omega(t) \|^2), \quad (24)$$

选择 ρ_1, ρ_2 使得 $c_2\rho_1 + c_4\rho_2 \leq \lambda_{\min}(\Omega_0)$, 能够得到

$$LV(\bar{x}(t), t) \leq \bar{x}^T(t) \Omega_0 \bar{x}(t) + \| e_\varepsilon(t) \| [c_1 + c_2 \| \hat{\omega}(t) \| + c_3 g_1(x(t), \mu(t)) + c_4 \| \hat{\omega}(t) \| g_2(x(t), \mu(t))] - \beta \| e_\varepsilon(t) \|^2 [2 + \| \hat{\omega}(t) \|^2 + g_1^2(x(t), \mu(t)) + \| \hat{\omega}(t) \|^2 g_2^2(x(t), \mu(t))] - \alpha(\beta(t) - \beta^*) \beta(t) + \frac{1}{2} c_2 \rho_1 \| e_\varepsilon(t) \|^2 + \frac{1}{2} c_4 \rho_2 \| e_\varepsilon(t) \|^2 g_2^2(x(t), \mu(t)). \quad (25)$$

再一次使用 Young's 不等式 得到

$$LV(\bar{x}(t), t) \leq \bar{x}^T(t) \Omega_0 \bar{x}(t) - (\beta^* - \frac{1}{2} c_2 \rho_1) \| e_\varepsilon(t) \|^2 - (\beta^* - \frac{1}{2} c_4 \rho_2) \| e_\varepsilon(t) \|^2 g_2^2(x(t), \mu(t)) + \alpha(\beta(t) - \beta^*) \beta(t) + \frac{1}{4\beta^*} (c_1^2 + c_2^2 + c_3^2 + c_4^2). \quad (26)$$

当 $\beta^* \geq \max\{c_2\rho_1, c_4\rho_2\}/2$, $-2(\beta(t) - \beta^*) \beta(t) \leq -(\beta(t) - \beta^*)^2 + (\beta^*)^2$, 可以得到

$$LV(\bar{x}(t), t) \leq \bar{x}^T(t) \Omega_0 \bar{x}(t) + \gamma, \quad (27)$$

其中: $\Omega_0 = A^T P + PA + B^T P B$, $\gamma = \frac{1}{4\beta^*} (c_1^2 + c_2^2 + c_3^2 + c_4^2) + \frac{1}{2} \alpha \beta^*$. 当 $\Omega_0 < 0$ 时 则存在 $\sigma > 0$ 使得

$\Omega_0 \Rightarrow \Omega_0 + \sigma I$ 定义函数 $k = \lambda_{\min}(P) \| \bar{x} \|^p$, $p = 2$ 且 $\mu = \frac{\sigma}{\lambda_{\max}(P)}$, 使得

$$k(\|x\|^p) = \lambda_{\min}(P) \|x\|^2 \leq V(\bar{x}(t), t), \quad (28)$$

$$LV(\bar{x}(t), t) \leq -\mu V(\bar{x}(t), t) + \gamma. \quad (29)$$

根据引理 1, 复合系统(18) 是依均方渐近有界的.

接下来 将证明当 $\delta(t) \neq 0$ 时复合系统是依均方渐近有界的. 考虑如下的辅助函数

$$J(t) = E \int_0^t [y^T(s) y(s) - \tau^2 \delta^T(s) \delta(s)] ds =$$

$$E \int_0^t [y^T(s) y(s) - \tau^2 \delta^T(s) \delta(s) + LV(\bar{x}(s), s)] ds - EV(\bar{x}(t), t) \leq$$

$$E \int_0^t [y^T(s) y(s) - \tau^2 \delta^T(s) \delta(s) + LV(\bar{x}(s), s)] ds \leq$$

$$E \int_0^t [y^T(s) y(s) - \tau^2 \delta^T(s) \delta(s) + \bar{x}^T(s) \Omega_0 \bar{x}(s) + \gamma] ds = E \int_0^t [Z(s)^T \Omega_1 Z(s) + \gamma] ds, \quad (30)$$

其中:

$$Z(s) = \begin{bmatrix} \bar{x}(s) \\ \delta(s) \end{bmatrix}, \Omega_1 = \begin{bmatrix} \Omega_0 + C^T C & PH \\ H^T P & -\tau^2 I \end{bmatrix}.$$

下面证明 $\Omega < 0 \Leftrightarrow \Omega_1 < 0$. 根据 Schur 补定理 $\Omega_1 < 0$ 等价于 $\Omega_2 < 0$,

$$\Omega_2 = \begin{bmatrix} \Xi_1 & 0 & 0 & B_1^T & B_1^T & C_1^T & 0 & 0 & 0 \\ * & \Xi_2 & Q_2 B_0 V - L_1^T Q_3 & 0 & 0 & C_2^T & 0 & 0 & 0 \\ * & * & \Xi_3 & 0 & 0 & C_3^T & 0 & 0 & Q_3 H_1 \\ * & * & * & -Q_1^{-1} & 0 & 0 & 0 & 0 & 0 \\ * & * & * & * & -Q_2^{-1} & 0 & 0 & 0 & 0 \\ * & * & * & * & * & -I & 0 & 0 & 0 \\ * & * & * & * & * & * & -\tau^2 I & 0 & 0 \\ * & * & * & * & * & * & * & -\tau^2 I & 0 \\ * & * & * & * & * & * & * & * & -\tau^2 I \end{bmatrix} < 0, \quad (31)$$

其中

$$\Xi_1 = (A_0 + B_0 K)^T Q_1 + Q_1 (A_0 + B_0 K), \Xi_2 = (A_0 - L_0)^T Q_2 + Q_2 (A_0 - L_0), \Xi_3 = G^T Q_3 + Q_3 G.$$

接下来, Ω_2 分别左乘和右乘 $\text{diag}\{X \ I \ I \ I \ Q_2 \ I \ I \ I \ I\}$ 得到 $\Omega_2 < 0 \Leftrightarrow \Omega_3 < 0$,

$$\Omega_3 = \begin{bmatrix} \Lambda_1 & 0 & 0 & X B_1^T & X B_1^T & X C_1^T & 0 & 0 & 0 \\ * & \Lambda_2 & Q_2 B_0 V - R_3 & 0 & 0 & C_2^T & 0 & 0 & 0 \\ * & * & \Lambda_3 & 0 & 0 & C_3^T & 0 & 0 & Q_3 H_1 \\ * & * & * & -X & 0 & 0 & 0 & 0 & 0 \\ * & * & * & * & -Q_2 & 0 & 0 & 0 & 0 \\ * & * & * & * & * & -I & 0 & 0 & 0 \\ * & * & * & * & * & * & -\tau^2 I & 0 & 0 \\ * & * & * & * & * & * & * & -\tau^2 I & 0 \\ * & * & * & * & * & * & * & * & -\tau^2 I \end{bmatrix} < 0, \quad (32)$$

其中

$$\Lambda_1 = A_0 X + X A_0^T + B_0 R_1 + R_1^T B_0^T, \Lambda_2 = A_0^T Q_2 + Q_2 A_0 - R_2^T - R_2, \Lambda_3 = G^T Q_3 + Q_3 G.$$

在式(32)中,当 $L_0 = Q_1^{-1} R_2, L_1 = (R_3 Q_3^{-1})^T, K = R_1 X^{-1}$ 从而得到 $\Omega_3 < 0 \Leftrightarrow \Omega < 0$.

综上所述,显然可以得到 $\Omega < 0 \Leftrightarrow \Omega_3 < 0 \Leftrightarrow \Omega_2 < 0 \Leftrightarrow \Omega_1 < 0$.此外,由 $\Omega_1 < 0$ 保证了 $\Omega_0 < 0$,由引理 1 可得复合系统(18)是依均方渐近有界的.证毕.

4 仿真例子

本节给出一个仿真算例来验证所提策略的有效性.考虑随机系统(1)带有如下的系统矩阵:

$$A_0 = \begin{bmatrix} -0.5 & -10 \\ 1 & -1.8 \end{bmatrix}, B_0 = \begin{bmatrix} -0.2 \\ 0.26 \end{bmatrix}, B_1 = \begin{bmatrix} -0.8 & -1 \\ 0 & -1.2 \end{bmatrix}.$$

非谐波干扰 $D(t)$ 表示如下:

$$\dot{\omega}_1(t) = \omega_2(t), \dot{\omega}_2(t) = -\frac{2}{1 + e^{\omega_2}} + (\omega_1 + \omega_2) \cos(x_1 + x_2 + u + x_1 x_2), \quad (33)$$

且 $V = [1 \ 1], H_1 = [0.1 \ 0.1]^T$.非线性函数 $\varphi(\hat{\omega}(t) \ x(t) \ \mu(t))$ 定义如下:

$$\varphi(\hat{\omega}(t) \ x(t) \ \mu(t)) = 2 + \|\hat{\omega}(t)\|^2 + \cos^2(x_1 + x_2 + u + x_1 x_2) + \|\hat{\omega}(t)\|^2 \cos^2(x_1 + x_2 + u + x_1 x_2).$$

$\delta_1(t)$ 为正弦波信号.加权矩阵 $C = [C_1 \ C_2 \ C_3], C_1 = [0.3 \ 0.1], C_2 = [0.4 \ 0.3], C_3 = [0.2 \ 0.1]$.

系统状态的初始值 $x(0) = [2 \ 1]^T$.在 Matlab 仿真中,使 $\xi(t)$ 为有界的白噪声.利用 Matlab 下的 LMI 工具箱,根据定理 1,可以得到

$$Q_1 = \begin{bmatrix} 2.7268 & 0.9056 \\ 0.9056 & 5.3328 \end{bmatrix}, Q_2 = \begin{bmatrix} 1.1949 & 0 \\ 0 & 1.1949 \end{bmatrix}, Q_3 = \begin{bmatrix} 1.3176 & 0.2572 \\ 0.2572 & 0.3029 \end{bmatrix},$$

$$L_1 = \begin{bmatrix} 0.0000 & -1.7480 \\ -7.2520 & -1.3000 \end{bmatrix}, L_2 = \begin{bmatrix} -0.0328 & 0.0426 \\ -0.7611 & 0.9894 \end{bmatrix}, K = [13.6470 \quad 1.4086].$$

仿真结果见图 1~3.

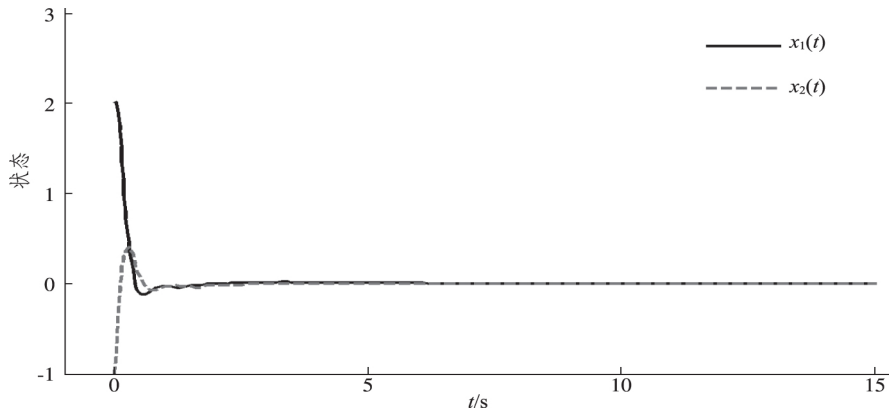


图 1 系统状态响应曲线

Fig.1 System state response curve

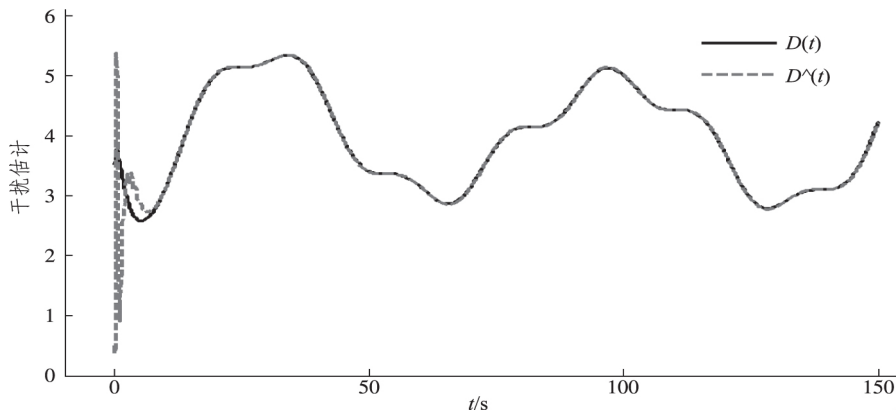


图 2 干扰估计曲线

Fig.2 Disturbance estimation curve

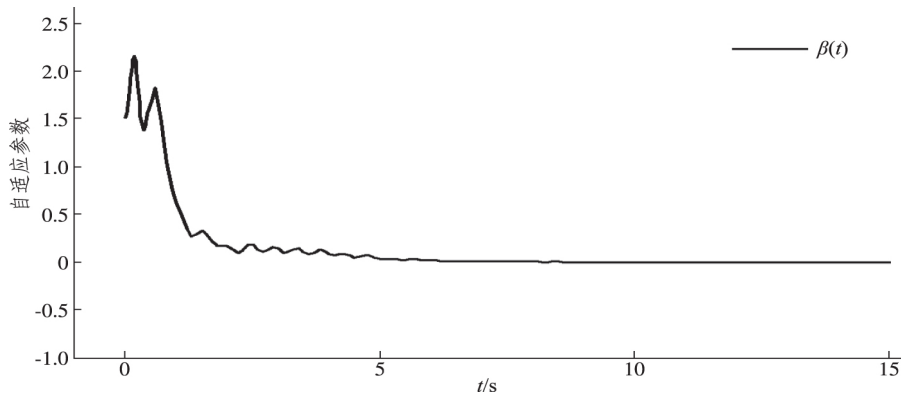


图 3 自适应参数曲线

Fig.3 Adaptive parameter curve

图 1 展现了在所提控制策略下随机系统的状态响应曲线,图 2 是干扰的追踪曲线,图 3 为自适应参数曲线.仿真结果表明了所提出的控制方法得到的结果是理想的,它保证了复合系统的状态最终达到依均方渐近有界.

5 结语

本文研究了一类带有多源异质干扰的随机系统的抗干扰控制问题,重点研究了系统状态与控制输入耦合的非谐波干扰.基于 DOBC 方法和自适应技术提出了基于自适应非线性干扰观测器的抗干扰控制策略,保证了复合系统能够达到依均方渐近有界.然而,本文所考虑的随机系统只包含了乘性噪声,下一步的研究工作将解决同时考虑加性噪声和乘性噪声的随机系统.

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ing body were analyzed. The experimental result shows that the increase of the revolving body's water entry angle can increase the splash crown's volume. At the same time, it can weaken the asymmetry of the cavity's walls. The larger the angle of entering the water is, the later the cavity at the tail of the revolving body forms. When the water entry angle is sufficiently small, the cavities at the revolving body's head and tail fall off respectively. The larger the angle of entering the water is, the smaller the resultant force acting on the revolving body is, then the smaller the acceleration is. Compared with the revolving body with streamline head, the revolving body with flat head makes flow separation more intense.

Keywords: revolving body; slamming; water entry angle; fluid field characteristics; motion characteristics

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Anti-disturbance Control Based on Adaptive Nonlinear Disturbance Observer for a Class of Stochastic Systems

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Abstract: The anti-disturbance control problem was investigated for a class of stochastic systems with multiple heterogeneous disturbances in this paper. The multiple heterogeneous disturbances include white noise and non-harmonic disturbances coupled with system state and control input. An adaptive nonlinear disturbance observer was designed to estimate non-harmonic disturbances. On this basis, an adaptive nonlinear disturbance observer-based control was proposed. Simulation example was given to show its effectiveness of the proposed method.

Keywords: stochastic system; multiple heterogeneous disturbances; anti-disturbance control; adaptive nonlinear disturbance observer

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